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ZHCSK82-SEPTEMBER 2019

具有内部基准的 TMCS1101 精度、隔离式电流传感器

Technical

Documents

1 特性

- 总误差电流感应: < 1.5%
 - 灵敏度误差: ±0.3%, -40℃ 至 +125℃
 - 失调电压误差: ±12.5mA, -40℃ 至 +125℃
 - 失调电流漂移: 0.02mA/°C
 - 温度范围内的线性度: 0.1% 典型值
- 已计划申请 UL1577、VDE 0884-11、60950 认证
 - 600V_{DC}/V_{PK} 工作隔离电压
 - 3kV_{RMS} 可承受的隔离电压
 - 双向和单向线性电流感应
- 零漂移内部基准
- 工作电源电压范围: 3V 至 5.5V
- 信号带宽: 80kHz
- 多个灵敏度选项:
 - TMCS1101A1U/B: 50mV/A
 - TMCS1101A2U/B: 100mV/A
 - TMCS1101A3U/B: 200mV/A
 - TMCS1101A4U/B: 400mV/A

2 应用范围

- 电机和负载控制
- 逆变器和 H 桥电流测量
- 功率因数校正
- 过流保护
- 直流和交流电源监控

3 说明

🥭 Tools &

Software

TMCS1101 是一款电隔离霍尔效应电流传感器,能够 测量直流或交流电流,并具有高精度、出色的线性度和 温度稳定性。低漂移、温度补偿信号链可以在器件的整 个温度范围内实现 < 1.5% 的满量程误差。

Support &

Community

22

输入电流流经内部 1.8mΩ 导体,此导体会产生一个由 集成式霍尔效应传感器测量的磁场。这种结构省去了外 部集中器并简化了 PCB 设计。低导体电阻可最大限度 减少功率损耗和热耗散。固有的电镀绝缘在电流路径与 电路之间提供了 600V 基本工作隔离电压和 3kV 电介 质可承受隔离电压。集成式电气屏蔽可提供出色的共模 抑制和瞬态抗扰度保护。

输出电压与输入电流成正比,并具有四个灵敏度选项。 固定的灵敏度允许 TMCS1101 使用单个 3V 至 5.5V 的电源运行,因此消除了比例式误差并提高了电源噪声 抑制能力。当电流流入到正输入引脚时,电流极性被视 为正极。可提供单向和双向感应型号。

TMCS1101 消耗的最大电源电流为 5mA,所有灵敏度 选项的额定工作温度范围都是 -40℃ 至 +125℃。

	器件信息 ⁽¹⁾	
器件型号	封装	封装尺寸(标称值)
TMCS1101	SOIC (8)	4.90mm x 3.90mm

(1) 如需了解所有可用封装,请参阅数据表末尾的封装选项附录。

典型应用





Texas Instruments

目录

1	特性	
2	应用	范围1
3	说明	1
4	修订	历史记录 2
5	Dev	ice Comparison Table 3
6	Pin	Configuration and Functions 3
7	Spe	cifications 4
	7.1	Absolute Maximum Ratings 4
	7.2	ESD Ratings 4
	7.3	Recommended Operating Conditions 4
	7.4	Thermal Information 4
	7.5	Insulation Specifications5
	7.6	Electrical Characteristics 6
8	Para	ameter Measurement Information
	8.1	Accuracy Parameters9
9	Deta	ailed Description 12
	9.1	Overview 12
	9.2	Functional Block Diagram 12

	9.3	Feature Description	12
	9.4	Device Functional Modes	17
10	App	lication and Implementation	. 18
	10.1	Application Information	18
	10.2	Typical Application	24
11	Pow	er Supply Recommendations	. 26
12	Layo	out	. 26
	12.1	Layout Guidelines	26
	12.2	Layout Example	27
13	器件	和文档支持	. 28
	13.1	器件支持	28
	13.2	文档支持	28
	13.3	接收文档更新通知	28
	13.4	支持资源	28
	13.5	商标	28
	13.6	静电放电警告	28
	13.7	Glossary	28
14	机械	、封装和可订购信息	. 28

4 修订历史记录

日期	修订版本	说明
2019 年9 月	*	初始发行版



5 Device Comparison Table

PRODUCT	SENSITIVITY	ZERO CURRENT OUTPUT VOLTAGE,	IIN LINEAR MEASUREMENT RANGE ⁽¹⁾	
	ΔV _{OUT} / ΔI _{IN+, IN-}	V _{OUT,0A}	V _S = 5 V	V _S = 3.3 V
TMCS1101A1B	50 mV/A		±46 A ⁽²⁾	±29 A ⁽²⁾
TMCS1101A2B	100 mV/A	0.5 × V _S	±23 A ⁽²⁾	±14.5 A
TMCS1101A3B	200 mV/A		±11.5 A	±7.25 A
TMCS1101A4B	400 mV/A		±5.75 A	±3.625 A
TMCS1101A1U	50 mV/A		-9 A \rightarrow 86 A ⁽²⁾	$-5.6~\text{A} \rightarrow 55.4 \text{A}^{(2)}$
TMCS1101A2U	100 mV/A	0.1)/	-4.5 A \rightarrow 43A ⁽²⁾	–2.8 A \rightarrow 27.7 A ⁽²⁾
TMCS1101A3U	200 mV/A	0.1 × V _S	$-2.25 \text{ A} \rightarrow 21.5 \text{ A}^{(2)}$	$-1.4 \text{ A} \rightarrow 13.85 \text{ A}$
TMCS1101A4U	400 mV/A		$-1.12 \text{ A} \rightarrow 10.75 \text{ A}$	$-0.7 \text{ A} \rightarrow 6.92 \text{ A}$

(1) Linear range limited by swing to supply and ground.

(2) Current levels must remain below both allowable continuous DC/RMS and transient peak current safe operating areas.

6 Pin Configuration and Functions



Pin Functions

PIN		1/0	DESCRIPTION
NO.	NAME	1/0	DESCRIPTION
1	IN+	Analog input	Input current positive pin
2	IN+	Analog input	Input current positive pin
3	IN–	Analog input	Input current negative pin
4	IN-	Analog input	Input current negative pin
5	GND	Analog	Ground
6	NC	No Connect	No connect
7	VOUT	Analog output	Output voltage
8	VS	Analog	Power supply

ADVANCE INFORMATION

Specifications 7

Absolute Maximum Ratings 7.1

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

			MIN	MAX	UNIT
Vs	Supply voltage		GND – 0.3	6	V
	NC Input	NC	GND – 0.3	$(V_{\rm S}) + 0.3$	V
	Analog output	VOUT	GND – 0.3	$(V_{S}) + 0.3$	V
TJ	Junction temperature		-65	150	°C
T _{stg}	Storage temperature		-65	150	°C

Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings (1) only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

7.2 ESD Ratings

			VALUE	UNIT
V _(ESD) E	Electrostatio discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V
	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±1000	V

JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process. (1)(2)JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V_{IN+}, V_{IN-} (1)	Input voltage	-600		600	V _{PK}
I _{IN} ⁽²⁾	Input current (Continuous dc or rms current)	-20		20	А
Vs	Operating supply voltage, TMCS1101A1B-3U, A1U-3U	3	5	5.5	V
Vs	Operating supply voltage, TMCS1101A4B, A4U	4.5	5	5.5	V
T _A	Operating free-air temperature	-40		125	°C

(1)

 V_{IN+} and V_{IN-} refer to the voltage at input current pins IN+ and IN-, relative to pin 5 (GND). Input current safe operating area is constrained by junction temperature. Recommended condition based on the TMCS1101EVM. Rating (2)is derated for elevated ambient temperatures.

Thermal Information 7.4

		TMCS1101	
	THERMAL METRIC ⁽¹⁾	D (SOIC)	UNIT
		8 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	36.6	°C/W
R _{0JC(top)}	Junction-to-case (top) thermal resistance	50.7	°C/W
$R_{ heta JB}$	Junction-to-board thermal resistance	9.6	°C/W
Ψ_{JT}	Junction-to-top characterization parameter	-0.1	°C/W
Ψ_{JB}	Junction-to-board characterization parameter	11.7	°C/W
R _{0JC(bot)}	Junction-to-case (bottom) thermal resistance	N/A	°C/W

For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application (1) report.

7.5 Insulation Specifications

	PARAMETER	TEST CONDITIONS	VALUE	UNIT
GENER	AL	I		-1
CLR	External clearance ⁽¹⁾	Shortest terminal-to-terminal distance through air	4	mm
CPG	External creepage ⁽¹⁾	Shortest terminal-to-terminal distance across the package surface	4	mm
DTI	Distance through the insulation	Minimum internal gap (internal clearance)	60	μm
CTI	Comparative tracking index	DIN EN 60112 (VDE 0303-11); IEC 60112	600	V
	Material group		II	
		Rated mains voltage ≤ 150 V _{RMS}	I-IV	
	Overvoltage category	Rated mains voltage ≤ 300 V _{RMS}	1-111	
		Rated mains voltage ≤ 600 V _{RMS}	1-11	
DIN V VI	DE V 0884-11:2017-01 ⁽²⁾			·
VIORM	Maximum repetitive peak isolation voltage	AC voltage (bipolar)	600	V _{PK}
		AC voltage (sine wave)	424	V _{RMS}
VIOWM	Maximum working isolation voltage	DC voltage	600	V _{DC}
VIOTM	Maximum transient isolation voltage	$V_{TEST} = V_{IOTM}$, t = 60 s (qualification); $V_{TEST} = 1.2 \times V_{IOTM}$, t = 1 s (100% production)	4242	V _{PK}
V _{IOSM}	Maximum surge isolation voltage ⁽³⁾	Test method per IEC 62368-1, 1.2/50 μ s waveform, V _{TEST} = 1.3 × V _{IOSM} (qualification)	6000	V _{PK}
		Method a: After I/O safety test subgroup 2/3, $V_{ini} = V_{IOTM}$, $t_{ini} = 60$ s; $V_{pd(m)} = 1.2 \times V_{IORM}$, $t_m = 10$ s	5	
q _{pd}	Apparent charge ⁽⁴⁾	Method a: After environmental tests subgroup 1, $V_{ini} = V_{IOTM}$, $t_{ini} = 60$ s; $V_{pd(m)} = 1.2 \times V_{IORM}$, $t_m = 10$ s	5	рС
		Method b3: At routine test (100% production) and preconditioning (type test) $V_{ini} = 1.2 \times V_{IOTM}$, $t_{ini} = 1$ s; $V_{pd(m)} = 1.2 \times V_{IOTM}$, $t_m = 1$ s	5	
	Pollution degree		2	
UL 1577	·	· · · · · ·		·
V _{ISO}	Withstand isolation voltage	$V_{TEST} = V_{ISO}$, t = 60 s (qualification); $V_{TEST} = 1.2 \times V_{ISO}$, t = 1 s (100% production)	3000	V _{RMS}

(1) Apply creepage and clearance requirements according to the specific equipment isolation standards of an application. Take care to maintain the creepage and clearance distance of the board design to make sure that the mounting pads of the isolator on the printed-circuit board do not reduce this distance. Creepage and clearance on a printed-circuit board become equal in certain cases. Techniques such as inserting grooves, ribs, or both on a printed circuit board are used to help increase these specifications.

(2) This coupler is for *basic electrical insulation* only within the maximum operating ratings. Compliance with the safety ratings is by means of protective circuits.

(3) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.

(4) Apparent charge is electrical discharge caused by a partial discharge (pd).

7.6 Electrical Characteristics

at $T_A = 25^{\circ}C$, $V_S = 5 V$,

	PARAMETERS	TEST CONDITIONS	MIN TYP	MAX	UNIT
OUTPUT					
Sensitivity		TMCS1101A1B	50		mV/A
		TMCS1101A2B	100		mV/A
		TMCS1101A3B	200		mV/A
		TMCS1101A4B	400		mV/A
	Sensitivity	TMCS1101A1U	50		mV/A
		TMCS1101A2U	100		mV/A
		TMCS1101A3U	200		mV/A
		TMCS1101A4U	400		mV/A
	Sensitivity error	$0.05~\textrm{V} \leq \textrm{V}_{\textrm{OUT}} \leq \textrm{V}_{\textrm{S}} - 0.2~\textrm{V}$	±0.15%	±0.5%	
	Sensitivity error	0.05 V \leq V _{OUT} \leq V _S – 0.2 V, T _A = –40°C to +125°C	±0.3%	±0.8%	
	Sensitivity error drift	$0.05 \text{ V} \le \text{V}_{\text{OUT}} \le \text{V}_{\text{S}} - 0.2 \text{ V}$	±20	±30	ppm/°C
		TMCS1101A1B	±1.6	±5	mV
		TMCS1101A2B	±1.8	±7.5	mV
		TMCS1101A3B	±1.8	±10	mV
	Output voltage affect array	TMCS1101A4B	±3	±18	mV
	Output voltage offset error	TMCS1101A1U	±1	±5	mV
		TMCS1101A2U	±1	±6	mV
		TMCS1101A3U	±2.6	±9	mV
V		TMCS1101A4U	±11	±25	mV
VOE		TMCS1101A1B, T _A = -40°C to +125°C	±2.2	±7.25	mV
		TMCS1101A2B, $T_A = -40^{\circ}C$ to +125°C	±2.5	±9	mV
		TMCS1101A3B, T _A = -40°C to +125°C	±3	±14	mV
	Output voltage offect error	TMCS1101A4B, T _A = -40°C to +125°C	±5	±23	mV
	Output voltage offset error	TMCS1101A1U, T _A = -40°C to +125°C	±1.2	±7.25	mV
		TMCS1101A2U, T _A = -40°C to +125°C	±1.2	±9	mV
		TMCS1101A3U, T _A = -40°C to +125°C	±6.4	±14	mV
		TMCS1101A4U, T _A = -40°C to +125°C	±14	±33	mV
		TMCS1101A1B	±32	±100	mA
		TMCS1101A2B	±18	±75	mA
		TMCS1101A3B	±9	±50	mA
	Offset error RTI ⁽¹⁾	TMCS1101A4B	±7.5	±45	mA
		TMCS1101A1U	±20	±100	mA
		TMCS1101A2U	±10	±60	mA
		TMCS1101A3U	±13	±45	mA
laa		TMCS1101A4U,	±27.5	±62.5	mA
IOS		TMCS1101A1B, T _A = -40°C to +125°C	±44	±145	mA
		TMCS1101A2B, T _A = -40°C to +125°C	±25	±90	mA
		TMCS1101A3B, T _A = -40°C to +125°C	±15	±70	mA
	Offact error PTI ⁽¹⁾	TMCS1101A4B, T _A = -40°C to +125°C	±12.5	±57.5	mA
		TMCS1101A1U, T _A = -40°C to +125°C	±24	±145	mA
		TMCS1101A2U, T _A = -40°C to +125°C	±12	±90	mA
		TMCS1101A3U, T _A = -40°C to +125°C	±32	±70	mA
		TMCS1101A4U, T _A = -40°C to +125°C	±35	±82.5	mA

⁽¹⁾ RTI = referred-to-input. Output voltage is divided by device sensitivity to refer signal to input current. See the *Parameter Measurement Information* section.



Electrical Characteristics (continued)

at $T_A = 25^{\circ}C$, $V_S = 5 V$,

	PARAMETERS	TEST CONDITIONS	MIN TYP	MAX	UNIT
		TMCS1101A1B, T _A = -40°C to +125°C	±86		µA/°C
		TMCS1101A2B, T _A = -40°C to +125°C	±44		µA/°C
		TMCS1101A3B, T _A = -40°C to +125°C	±35		µA/°C
	O(()) (1)	TMCS1101A4B, T _A = -40°C to +125°C	±30		µA/°C
	Offset error drift, R I 107	TMCS1101A1U, T _A = -40°C to +125°C	±60		µA/°C
		TMCS1101A2U, T _A = -40°C to +125°C	±36		µA/°C
		TMCS1101A3U, T _A = -40°C to +125°C	±29		µA/°C
		TMCS1101A4U, T _A = -40°C to +125°C	±20		µA/°C
	Nonlinearity error	$V_{OUT} = 0.5 \text{ V to } V_{S} - 0.5 \text{ V}$	±0.1%		
CMTI	Common mode transient immunity		25		kV/µs
CMRR	Common mode rejection ratio, RTI ⁽¹⁾		0.1		uA/V
	Zero current V _{OUT}	TMCS1101A<1-4>U	0.1*V _S		V/V
	Zero current V _{OUT}	TMCS1101A<1-4>B	0.5*V _S		V/V
		TMCS1101A1B	380		μA/√Hz
		TMCS1101A2B	330		μA/√Hz
		TMCS1101A3B	300		μA/√Hz
		TMCS1101A4B	225		μA/√Hz
	Noise density, RTI ⁽¹⁾	TMCS1101A1U	380		μA/√Hz
		TMCS1101A2U	330		μA/√Hz
		TMCS1101A3U	300		μA/√Hz
		TMCS1101A4U	225		μA/√Hz
INPUT	<u>-</u>			I	
R _{IN}	Input conductor resistance	IN+ to IN-	1.8		mΩ
	Input conductor resistance drift	T _A = -40°C to +125°C	7		μΩ/°C
G	Magnetic coupling factor	T _A = 25°C	1.2		mT/A
I _{IN}	Maximum continuous RMS current (2)	T _A = 25°C	30		А
I _{IN}	Maximum continuous RMS current (2)	T _A = 85°C	25		А
I _{IN}	Maximum continuous RMS current (2)	T _A = 105°C	22.5		А
I _{IN}	Maximum continuous RMS current (2)	T _A = 125°C	16		А
	NC (Pin 6) input impedance	Over allowable range, $GND < V_{NC} < V_{S}$	1		MΩ
VOLTAGE	OUTPUT			I	
_		f = 1 Hz to 1 kHz	0.2		Ω
Z _{OUT}	Closed loop output impedance	f = 10 kHz	2		Ω
	Maximum capacitive load	No sustained oscillation	1		nF
	Short circuit output current	VOUT short to ground, short to V _S	90		mA
	Swing to V _S power-supply rail	$R_L = 10 \text{ k}\Omega$ to GND, $T_A = -40^{\circ}\text{C}$ to $+125^{\circ}\text{C}$	V _S - 0.02	V _S – 0.1	V
	Swing to GND	$R_L = 10 \text{ k}\Omega \text{ to GND}, T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}$	5	10	mV
FREQUEN	CY RESPONSE			l	
BW	Bandwidth ⁽³⁾	–3-dB Bandwidth	80		kHz
	Nyquist Frequency ⁽³⁾		125		kHz
SR	Slew rate	Slew rate of output amplifier during single transient step.	1.5		V/µs
tr	Response time	Time between the input current step reaching 90% of final value to the sensor output reaching 90% of its final value, for a 1V output transition.	6.5		μs
t _p	Propagation delay	Time between the input current step reaching 10% of final value to the sensor output reaching 10% of its final value, for a 1V output transition.	4		μs

(2) Thermally limited by junction temperature. Applies when device mounted on TMCS1101EVM. For more details, see the *Safe Operating Area* section.

(3) Refer to the *Transient Response* section for details of frequency response of the device.

NSTRUMENTS

FEXAS

Electrical Characteristics (continued)

at $T_A = 25^{\circ}C$, $V_S = 5 V$,

	PARAMETERS	TEST CONDITIONS	MIN	ТҮР	MAX	UNIT
t _{r,SC}	Short-circuit response time	Time between the input current step reaching 90% of final value to the sensor output reaching 90% of its final value. Input current step amplitude is twice full scale linear range.		5		μs
t _{p,SC}	Short-circuit propagation delay	Time between the input current step reaching 10% of final value to the sensor output reaching 10% of its final value. Input current step amplitude is twice full scale linear range.		3		μs
POWER S	UPPLY					
	Quiescent ourrent	T _A = 25°C		4.25	5	mA
I _Q Quiescent current T		$T_A = -40^{\circ}C \text{ to } +125^{\circ}C$			6	mA



8 Parameter Measurement Information

8.1 Accuracy Parameters

The ideal first-order transfer function of the TMCS1101 is given by $\Delta \pm 1$, where the output voltage is a linear function of input current. The accuracy of the device is quantified both by the error terms in the transfer function parameters, as well as by nonidealities that introduce additional error terms not in the simplified linear model.

 $V_{OUT} = S * I_{IN} + V_{OUT,0A}$

where

- V_{OUT} is the analog output voltage.
- S is the ideal sensitivity of the device.
- I_{IN} is the isolated input current.
- V_{OUT.0A} is the zero current output voltage for the device variant.

(1)

8.1.1 Sensitivity, Sensitivity Error, and Drift

Sensitivity is the proportional change in the sensor output voltage due to a change in the input conductor current. This sensitivity is the slope of the first-order transfer function of the sensor, as shown in 🛽 1. The sensitivity of the TMCS1101 is tested and calibrated at the factory for high accuracy.



图 1. Sensitivity, Offset, and Nonlinearity Error

Deviation from ideal sensitivity is quantified by sensitivity error. Sensitivity error is defined as the percent variation of the best-fit measured sensitivity from the ideal sensitivity, based on the variant of the TMCS1101. When specified over a temperature range, this is the worst-case sensitivity error at any temperature within the range.

 $e_{S} = [(S_{fit} - S_{ideal}) / S_{ideal}] \times 100\%$

where

- e_s is the sensitivity error.
- S_{fit} is the best fit sensitivity.
- S_{Ideal} is the ideal sensitivity.

(2)

Texas Instruments

(3)

(5)

Accuracy Parameters (接下页)

Sensitivity error drift is the worst-case change in sensitivity error per degree Celsius change in ambient temperature. This parameter is reported in ppm/°C. To convert sensitivity error drift to a percentage for a given change in temperature, multiply the drift by the change in temperature and convert to percentage, as in $\Delta \vec{x}$ 3.

$$\mathbf{e}_{\mathbf{S},\Delta \mathsf{T}}\left(\%\right) = \mathbf{S}_{\mathsf{drift}}\left(\frac{\mathsf{ppm}}{^{\circ}\mathsf{C}}\right) \times \Delta \mathsf{T} \times 1000$$

where

- S_{drift} is the sensitivity error drift.
- ΔT is the temperature range from 25°C.

8.1.2 Offset Error and Drift

Offset error is the deviation from the ideal output voltage with zero input current through the device. Offset error can be referred to the output as a voltage error V_{OE} or referred to the input as a current offset error I_{OS} ; however, offset error is a single error source and must only be included once in error calculations.

The output voltage offset error of the TMCS1101 is the deviation of the measured V_{OUT} with zero input current from the ideal value of the zero current output voltage. This ideal voltage is either 10% of V_S for unidirectional devices (AxU) or 50% of V_S for bidirectional devices (AxB), as shown in $\Delta \pm 4$ and $\Delta \pm 5$, respectively.

$$V_{OE} = V_{OUT,0A} - V_S * 0.1$$
 (4)

$$V_{OE} = V_{OUT,0A} - V_{S} * 0.5$$

where

V_{OUT,0A} is the device output voltage with zero input current.

The total offset error includes multiple individual error sources: errors in the internal reference, the magnetic offset of the Hall sensor, and any offset voltage errors of the signal chain.

The input referred (RTI) offset error is the output voltage offset error divided by the sensitivity of the device, shown in $\Delta \vec{x}$ 6. Refer the offset error to the input of the device to allow for easier total error calculations and direct comparison to input current levels. However the calculations are done, the error sources quantified by V_{OE} and I_{OS} are the same, and must only be included once for error calculations.

$$I_{OS} = V_{OE} / S$$
(6)

Offset error specifications are defined at both room temperature and across the full temperature range. Offset error specified over a temperature range is the worst-case sensitivity error at any temperature within the range, and must not be considered as additive to room temperature offset error. Offset error drift is the worst-case rate of change in a device offset across the temperature spectrum, and is used to calculate maximum offset error across an arbitrary temperature range in the same manner as sensitivity drift, and as described in the *Total Error Calculation Examples* section.

8.1.3 Nonlinearity Error

Nonlinearity is the deviation of the output voltage from a linear relationship to the input current. Nonlinearity voltage, as shown in \mathbb{E} 1, is the maximum voltage deviation from the best-fit line based on measured parameters, calculated by $\Delta \pm 7$.

 $V_{NL} = V_{OUT,MEAS} - (I_{MEAS} \times S_{fit} + V_{OUT,0A})$

where

- V_{OUT,MEAS} is the voltage output at maximum deviation from best fit.
- I_{MEAS} is the input current at maximum deviation from best fit.
- S_{fit} is the best-fit sensitivity of the device.
- V_{OUT,0A} is the device zero current output voltage.

Nonlinearity error (e_{NL}) for the TMCS1101 is the nonlinearity voltage specified as a percentage of the full-scale output range (V_{FS}), as shown in $\Delta \pm 8$.

$$e_{NL} = 100\% * \frac{v_{NL}}{v_{FS}}$$

(8)

(7)

10



Accuracy Parameters (接下页)

8.1.4 External Magnetic Field Errors

The TMCS1101 does not have stray field-rejection capabilities, so external magnetic fields from adjacent highcurrent traces or nearby magnets can impact the output measurement. The total sensitivity (S) of the device is comprised of the initial transformation of input current to magnetic field quantified as the magnetic coupling factor (G), as well as the sensitivity of the Hall element and the analog circuitry that is factory calibrated to provide a final sensitivity. The output voltage is proportional to the input current by the device sensitivity, as defined in $\Delta \mathfrak{I}$ 9.

$$S = G * S_{Hall} * A_V$$

where

- S is the TMCS1101 sensitivity in mV/A.
- G is the magnetic coupling factor in mT/A.
- S_{Hall} is the senitivity of the Hall plate in mV/mT.
- A_V is the analog circuitry gain in V/V.

An external field, B_{EXT}, is measured by the Hall sensor and signal chain, in addition to the field generated by the leadframe current, and is added as an extra input term in the total output voltage function:

$$V_{OUT} = B_{EXT} * S_{Hall} * A_V + I_{IN} * G * S_{Hall} * A_V + V_{OUT,0A}$$

Observable from 公式 10 is that the impact of an external field is an additional equivalent input current signal, I_{BEXT} , shown in 公式 11. This effective additional input current has no dependence on Hall or analog circuitry sensitivity, so all gain variants have equivalent input-referred current error due to external magnetic fields.

$$I_{B_{EXT}} = \frac{B_{EXT}}{G}$$

(9)

(10)

(11)



9 Detailed Description

9.1 Overview

The TMCS1101 is a Hall-sensor-based precision current sensor, featuring a 600-V basic isolation working voltage, < 1.5% full-scale error across temperature, and device options providing both unidirectional and bidirectional current sensing. Input current flows through a conductor between the isolated input current pins. The conductor has a 1.8-m Ω resistance at room temperature for low power dissipation and a 20-A RMS continuous current handling capability up to 125°C ambient temperature on the TMCS1100EVM. The magnetic field generated by the input current is sensed by a Hall sensor and amplified by a precision signal chain. The device can be used for both ac and dc current measurements and has a bandwidth of 80 kHz. There are four fixed-sensitivity device variants for a wide option of linear sensing ranges, and the TMCS1101 can operate with a low voltage supply from 3 V to 5.5 V. The TMCS1101 is optimized for high accuracy and temperature stability, with both offset and sensitivity compensated across the entire operating temperature range.

9.2 Functional Block Diagram



9.3 Feature Description

9.3.1 Current Input

Input current to the TMCS1101 passes through the isolated side of the package leadframe through the IN+ and IN- pins. The current flow through the package generates a magnetic field that is proportional to the input current, and measured by a galvanically isolated, precision, Hall sensor IC. The low-ohmic leadframe path reduces power dissipation compared to alternative current measurement methodologies, and does not require any passive external components on the high-voltage side. In addition, no isolated supplies or control signals are needed on the high-voltage side, further simplifying implementation. As a result of the electrostatic shielding on the Hall sensor die, only the magnetic field generated by the input current is measured, thus limiting input voltage switching pass-through to the circuitry. This configuration allows for direct measurement of currents with high-voltage transients without signal distortion on the current-sensor output.

The current input leadframe conductor has a nominal resistance of 1.8 m Ω at 25°C. The leadframe is composed of copper; therefore, the leadframe has a positive temperature coefficient that causes resistance to increase at higher temperatures. A typical temperature coefficient is 3300 ppm/°C, causing a 33% rise in resistivity for every 100°C of leadframe temperature change from room temperature.



Feature Description (接下页)

9.3.2 Input Isolation

The separation between the input conductor and the Hall sensor die due to the TMCS1101 construction provides inherent galvanic isolation between package pins 1-4 and pins 5-8. Insulation capability is defined according to certification agency definitions and using industry-standard test methods as defined in the *Insulation Specifications* table. Assessment of device lifetime working voltages follow the VDE 0884-11 standard for basic insulation, requiring time-dependent dielectric breakdown (TDDB) data-projection failure rates of less than 1000 part per million (ppm), and a minimum insulation lifetime of 20 years. The VDE standard also requires an additional safety margin of 20% for working voltage, and a 30% margin for insulation lifetime, translating into a minimum required lifetime of 26 years at 509 V_{RMS}.



图 2. Insulation Lifetime

9.3.3 High-Precision Signal Chain

The TMCS1101 uses a precision, low-drift signal chain with proprietary sensor linearization techniques to provide a highly accurate and stable current measurement across the full temperature range of the device. The device is fully tested and calibrated at the factory to account for any variations in either silicon or packaging process variations. The full signal chain provides a fixed sensitivity voltage output that is proportional to the current through the leadframe of the isolated input.

TMCS1101

ZHCSK82-SEPTEMBER 2019



Feature Description (接下页)

9.3.3.1 Temperature Stability

System calibration at room temperature is a common practice for many applications. This initial calibration results in a very accurate measurement under the conditions at which calibration was performed because individual components of the total error are eliminated. As the ambient temperature changes as a result of device self-heating or environmental conditions, any drift in critical system parameters will reintroduce these errors into the system performance. For many systems, this drift in performance across temperature is the primary contributor to performance degradation at the system level. These variations in component parametric performance must be accounted for in total system error calculations. The TMCS1101 includes a proprietary temperature compensation technique, and results in best in industry parametric drift across the full temperature range. A zero-drift signal chain architecture and Hall sensor temperature stabilization methods enable stable sensitivity and minimize offset errors across temperature, and drastically improves system-level performance across the required operating conditions.





Feature Description (接下页)

9.3.3.2 Transient Response

The TMCS1101 signal chain is a discrete time-sampled system with a typical sampling frequency of 250 kHz. Any variation in the input current signal over this sampling period is averaged. As such, the device has an effective Nyquist frequency of 125 kHz. At the end of each integration cycle, the signal propagates through the remainder of the signal chain to the output. Depending on the alignment of a change in input current relative to the sampling window, the output might not settle to the final signal until the second integration cycle. If 6 shows a typical output waveform response to ramp and step input currents. For a slowly varying input current signal, the output is a discrete time representation with a phase delay of the integration sampling window.



图 6. Precision Signal-Chain Response Behavior

Transient response to an input current step is critical for overcurrent of fault-condition detection. As a result of the TMCS1101 discrete time signal chain, the transient response to step input events varies depending on the relative timing of the event to the sampling window. \mathbb{Z} 7 shows two transient waveforms to an input-current step event, but occurring at different times during the sampling interval. With *Vout1*, the event occurs near the beginning of the 4-µs sampling interval, so more of the high-current signal is averaged into the first 4-µs output value. If the event occurs closer to the end of the sampling interval, as with *Vout2*, the initial output response is smaller, but occurs closer to the input current step. In both cases, the full transition of the output takes two sampling intervals to reach the final output value. The timing of the current event relative to the sampling window determines the proportional amplitude of the first and second sampling intervals.



图 7. Transient Response to Input-Current Step Sufficient for 1-V Output Swing

TMCS1101

ZHCSK82-SEPTEMBER 2019

Feature Description (接下页)

The output value is effectively an average over the sampling window; therefore, a large-enough current transient can drive the output voltage to the full range in the first sample response. This condition is likely to be true in the case of a short-circuit or fault event. 🛽 8 shows an input-current step of 100 A, and the output response of an TMCS1101A3B. In the case of *Vout1*, the event occurs near the beginning of a sampling window, and so the output transitions to full scale in the first integrator output sample. In the case of *Vout2*, the event occurs near the end of an integration cycle, so there are two distinct output transitions. The relative timing and size of the input current transition determines whether the output transitions to full scale in a single cycle. In either case, the total response time is approximately one integration period.



图 8. Transient Response to a Large Input Current Step

9.3.4 Internal Reference Voltage

The device has an internal resistor divider from the analog supply V_S that determines the zero-current output voltage, $V_{OUT,OA}$. This zero-current output level along with sensitivity determine the measurable input current range of the device, and allows for unidirectional or bidirectional sensing, as described in Absolute Maximum Ratings. The TMCS1101AxB variants have a zero-current output set by $\Delta \vec{x}$ 12, while the TMCS1101AxU devices have a zero-current output voltage set by $\Delta \vec{x}$ 13.

$$V_{OUT,0A} = V_S \times 0.5$$
 (12)
 $V_{OUT,0A} = V_S \times 0.1$ (13)

These respective reference voltages enable a bidirectional measurable current range for the AxB devices and a unidirectional measurement range for the AxU devices, as shown in \mathbb{E} 9.



图 9. Output Voltage Relationship to Input Current for TMCS1101A2B and TMCS1101A2U



Feature Description (接下页)

9.3.5 Current-Sensing Measurable Ranges

The TMCS1101 measurable input current range depends on the device variant, as well as the analog supply V_s . The output voltage is a first-order linear function of the input current, as shown in $\Delta \pm 1$, and is only limited by V_{OUT} swing to either supply or ground. The linear output swing range to both V_s and GND is calculated by equations $\Delta \pm 14$ and $\Delta \pm 15$.

 $V_{OUT,max} = V_S - Swing_{VS}$ (14) $V_{OUT,min} = Swing_{GND}$ (15)

Rearranging the transfer function of the device to solve for input current and substituting $V_{QUT,max}$ and $V_{OUT,min}$ yields maximum and minimum measurable input current ranges described by $\Delta \pm 16$ and $\Delta \pm 17$.

$$I_{IN,MAX+} = (V_{OUT,max} - V_{OUT,0A}) / S$$
$$I_{IN,MAX-} = (V_{OUT,0A} - V_{OUT,min}) / S$$

where

- I_{IN,MAX+} is the maximum linear measurable positive input current.
- I_{IN.MAX-} is the maximum linear measurable negative input current.
- S is the sensitivity of the device variant.
- V_{OUT,0A} is the appropriate zero current output voltage.

TMCS1101A<1-4>B variants accommodate bidirectional current sensing by creating zero-current output voltage equal to half of the supply (V_S) potential, while TMCS1101A<1-4>U variants provide most of the dynamic measurable range for positive currents.

9.4 Device Functional Modes

9.4.1 Power-Down Mode

As a result of the inherent galvanic isolation of the device, very little consideration must be paid to powering down the device, as long as the limits in the *Absolute Maximum Ratings* table are not exceeded on any pins. The isolated current input and the low-voltage signal chain can be decoupled in operational behavior, as either can be energized with the other shut down, as long as the isolation barrier capabilities are not exceeded. The low-voltage power supply can be powered down while the isolated input is still connected to an active high-voltage signal or system.

(16)

(17)

10 Application and Implementation

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Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

10.1 Application Information

The key feature sets of the TMCS1101 provide significant advantages in any application where an isolated current measurement is required.

- Galvanic isolation provides a high isolated working voltage and excellent immunity to input voltage transients.
- Hall based measurement simplifies system level solution without the need for a power supply on the high voltage (HV) side.
- An input current path through the low impedance conductor minimizes power dissipation.
- Excellent accuracy and low temperature drift eliminate the need for multipoint calibrations without sacrificing system performance.
- A wide operating supply range enables a single device to function across a wide range of voltage levels.

These advantages increase system-level performance while minimizing complexity for any application where precision current measurements must be made on isolated currents. Specific examples and design requirements are detailed in the following section.



Application Information (接下页)

10.1.1 Total Error Calculation Examples

Total error can be calculated for any arbitrary device condition and current level. Error sources considered should include input-referred offset current, power-supply rejection, input common-mode rejection, sensitivity error, nonlinearity, and the error caused by any external fields. Compare each of these error sources in percentage terms, as some are significant drivers of error and some have inconsequential impact to current error. Offset (公式 18), CMRR (公式 19), PSRR (公式 20), and external field error (公式 21) are all referred to the input, and so, are divided by the actual input current I_{IN} to arrive percentage errors. For calculations of sensitivity error and nonlinearity error, the percentage limits explicitly specified in the *Electrical Characteristics* table can be used.

$$e_{l_{OS}}(\%) = \frac{I_{OS}}{I_{IN}}$$

$$e_{CMRR}(\%) = \left| \frac{CMRR * V_{CM}}{I_{IN}} \right|$$

$$e_{PSRR}(\%) = \left| \frac{PSRR * (V_S - 5)}{I_{IN}} \right|$$

$$e_{B_{EXT}}(\%) = \frac{\left| \frac{B_{EXT}}{G} \right|}{I_{IN}}$$

$$(21)$$

When calculating error contributions across temperature, only the input offset current and sensitivity error contributions vary significantly. In both cases, specifications for both the maximum device temperature range and the parameter drift across temperature are provided. For determining actual performance limits across a narrower temperature range than the specified -40°C to +125°C, use $\Delta \pm 22$ and $\Delta \pm 23$ for offset error and sensitivity error, respectively. In both of these calculations, the maximum specified drift for the parameter can be multiplied by the desired temperature deviation from room temperature (ΔT). Use the smaller value of this drift calculation and the specified range over the full temperature range. The sensitivity drift ($e_{S,drift}$) is specified in ppm/°C, and must be converted to percentage error.

$$\mathbf{e}_{\mathbf{I}_{OS,\Delta T}}(\%) = \frac{\min\left[\mathbf{I}_{OS,RT} + \mathbf{I}_{OS,drift} * \Delta T; \mathbf{I}_{OS,FT}\right]}{\mathbf{I}_{IN}}$$
(22)
$$\mathbf{e}_{S_{\Delta T}}(\%) = \min\left[\mathbf{e}_{S} + \mathbf{e}_{S,drift} * 1000 * \Delta T; \mathbf{e}_{S,FT}\right]$$
(23)

In order to accurately calculate the total expected error of the device, the contributions from each of the individual components above must be understood in reference to operating conditions. There are two separate ways to calculate total error for any particular system. In a worst case scenario, each error term would be at its absolute maximum with the same polarity. In such a case, the total system error would be a mathematical summation of each individual error source, as shown in $\Delta \pm 24$ for room temperature. For across temperature worst case error, the input referred offset and sensitivity error for the relevant range should be substituted in place of the room temperature values, as in $\Delta \pm 25$.

$$\mathbf{e}_{\text{worst}}(\%) = \mathbf{e}_{\text{I}_{OS}} + \mathbf{e}_{\text{PSRR}} + \mathbf{e}_{\text{CMRR}} + \mathbf{e}_{\text{B}_{\text{EXT}}} + \mathbf{e}_{\text{S}} + \mathbf{e}_{\text{NL}}$$
(24)

$$\mathbf{e}_{\text{worst},\Delta T}(\%) = \mathbf{e}_{\mathsf{I}_{OS,\Delta T}} + \mathbf{e}_{PSRR} + \mathbf{e}_{CMRR} + \mathbf{e}_{\mathsf{B}_{\mathsf{EXT}}} + \mathbf{e}_{\mathsf{S},\Delta T} + \mathbf{e}_{\mathsf{NL}}$$
(25)

Because the statistical probability of any device actually existing in this worst case corner is insignificant, a better methodology is to use a root sum squared (RSS) calculation for uncorrelated error sources. This method takes into account the statistically uncorrelated nature of the individual error terms to provide a more realistic total error based on the distributions of each error component. For the TMCS1101, only the input referred offset current (I_{OS}), CMRR, and PSRR are statistically correlated. These error terms are lumped in an RSS calculation in order to reflect this nature, as shown in $\Delta \vec{x}$ 26 for room temperature and $\Delta \vec{x}$ 27 for across a given temperature range.

$$e_{\text{RSS}}(\%) = \sqrt{\left(e_{\text{I}_{\text{OS}}} + e_{\text{PSRR}} + e_{\text{CMRR}}\right)^2 + e_{\text{B}_{\text{EXT}}}^2 + e_{\text{S}}^2 + e_{\text{NL}}^2}$$
(26)



Application Information (接下页)

$$\mathbf{e}_{\text{RSS},\Delta T}(\%) = \sqrt{\left(\mathbf{e}_{\text{I}_{\text{OS},\Delta T}} + \mathbf{e}_{\text{PSRR}} + \mathbf{e}_{\text{CMRR}}\right)^2 + \mathbf{e}_{\text{B}_{\text{EXT}}}^2 + \mathbf{e}_{\text{S},\Delta T}^2 + \mathbf{e}_{\text{NL}}^2}$$
(27)

The total error calculation has a strong dependence on the actual input current; therefore, always calculate total error across the dynamic range that is required. These curves asymptotically approach the sensitivity and nonlinearity error at high current levels, and approach infinity at low current levels because of error terms with input current in the denominator. Key figures of merit for any current-measurement system include the total error percentage at full-scale current, as well as the dynamic range of input current over which the error remains below some key level. \mathbb{B} 10 illustrates the total RSS error as a function of input current for a TMCS1101A2B at room temperature and across the full temperature range with V_S of 5 V.



图 10. RSS Error vs Input Current



Application Information (接下页)

10.1.1.1 Room Temperature Error Calculations

For room-temperature total-error calculations, specifications across temperature and drift are ignored. As an example, consider a TMCS1101A2B with a supply voltage (V_S) of 3.3 V and a worst-case common-mode excursion of 600 V to calculate operating-point-specific parameters. Consider a measurement error due to an external magnetic field of 30 μ T, roughly the Earth's magnetic field strength. The full-scale current range of the device in specified conditions is slightly greater than 15 A; therefore, calculate error at both 15 A and 7.5 A to highlight error dependence on the input-current level. $\frac{1}{5}$ 1 shows the individual error components, and the worst-case and RSS total error calculations at room temperature under the conditions specified. Relative to other errors, the additional error from CMRR and PSRR are negligible, and can typically be ignored for total error calculations.

ERROR COMPONENT	SYMBOL	EQUATION	% TOTAL ERROR AT I _{IN} = 15 A	% TOTAL ERROR AT I _{IN} = 7.5 A
Input offset error	e _{los}	$e_{I_{OS}}(\%) = \frac{I_{OS}}{I_{IN}}$	0.5%	1.0%
CMRR error	e _{CMRR}	$e_{CMRR}(\%) = \left \frac{CMRR * V_{CM}}{I_{IN}} \right $	0.00%	0.01%
External Field error	e _{Bext}	$e_{B_{EXT}}(\%) = \frac{\left \frac{B_{EXT}}{G}\right }{I_{IN}}$	0.17%	0.33%
Sensitivity error	e _S	Specified in Electrical Characteristics	0.5%	0.5%
Nonlinearity error	e _{NL}	Specified in Electrical Characteristics	0.1%	0.1%
Worst-case total error	e _{worst}	e_{worst} (%) = $e_{I_{OS}} + e_{PSRR} + e_{CMRR} + e_{B_{EXT}} + e_{S} + e_{NL}$	1.3%	2%
RSS total error	e _{RSS}	$e_{RSS}(\%) = \sqrt{\left(e_{I_{OS}} + e_{PSRR} + e_{CMRR}\right)^2 + e_{B_{EXT}}^2 + e_{S}^2 + e_{NL}^2}$	0.74%	1.19%

表 1. Total Error Calculation: Room Temperature Example



10.1.2 Safe Operating Area

The isolated input current safe operating area (SOA) of the TMCS1101 is constrained by input conductor thermal dissipation causing die junction temperature to exceed maximum T_J rating of 150°C. Continuous current capability refers to the ability of the device to conduct a given dc or rms current (if a periodic or ac waveform) continuously through the device at a given ambient temperature. The TMCS1101 can tolerate much higher transient short-duration currents, which are limited by different thermal mechanisms, such as fusing of the leadframe. These mechanisms depend on pulse duration, amplitude, and device thermal states.

Current capability for both rms and short-duration pulses depend on the thermal environment and design of the system-level board. All thermal and SOA ratings are for a single TMCS1101 device on the TMCS1100EVM, with no air flow in the specified ambient temperature conditions. Device use profiles must satisfy both continuous conduction and short-duration transient SOA capabilities for the thermal environment under which the system will be operated.

10.1.2.1 Continuous-Current Capability

The continuous-current capability of the TMCS1101 is constrained by the maximum junction temperature because of the power dissipation in the input conductor and die. Multiple thermal variables control the transfer of heat from the device to the surrounding environment, including air flow, ambient temperature, and PCB construction and design. The longest thermal time constants of the device packaging and board are on the order of seconds; therefore, any continuous periodic waveform with a frequency higher than 1 Hz can be evaluated based on the rms continuous-current level.

The continuous-current capability is thermally constrained; therefore, the capability of the device varies across the operating ambient temperature range. ▲ 11 shows the maximum current-handling capability of the device on the TMCS100EVM. Current capability falls off at higher ambient temperatures because of the reduced thermal transfer from junction-to-ambient and a leadframe positive temperature coefficient that causes increased power dissipation. By improving the thermal design of an application the SOA can be extended to higher currents at elevated temperatures. Using larger and heavier copper power planes, providing air flow over the board, or adding heat sinking structures to the area of the device can all improve thermal performance.



图 11. Maximum Continuous RMS Current vs Ambient Temperature



10.1.2.2 Short-Duration Current Capability

Higher-current events that are shorter duration can be tolerated by the TMCS1101, because the junction temperature does not reach thermal equilibrium within the pulse duration. 12 shows the short-circuit duration curve for the device for single current-pulse events, where the leadframe resistance changes after stress. This level is reached before a leadframe fusing event, but is a fundamental limit to current-handling capability of the leadframe. For long-duration pulses, the current capability approaches the continuous rms limit at the given ambient temperature. For repetitive pulsed events, the current levels must satisfy both the short-duration current capability and the rms continuous current levels for the duration of the subsequent pulse events.



图 12. Single-Pulse Leadframe Capability

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10.2 Typical Application

Inline sensing of motor phase current provides significant benefits to the performance of a motor control system, allowing advanced control algorithms and diagnostics with minimal postprocessing. A primary challenge to inline sensing for motor drives is that the current sensor is subjected to full HV supply-level PWM transients driving the motor phase. The inherent isolation of an in-package Hall-effect current sensor topology helps overcome this challenge, providing high common-mode immunity, as well as isolation between the high-voltage motor drive levels and the low-voltage control circuitry. 🕅 13 illustrates the use of the TMCS1101 in such an application.



图 13. Inline Motor Phase Current Sensing

10.2.1 Design Requirements

For current sensing of a three-phase motor application, make sure to provide linear sensing across the expected current range, and make sure that the device remains within working thermal constraints. A single TMCS1101 for each phase can be used, or two phases can be measured, and the third phase calculated on the motor-controller host processor. For this example, consider a nominal supply of 5 V but a minimum of 4.9 V to include for some supply variation. Maximum output swings are defined according to TMCS1101 specifications, and a full-scale current measurement of ±20 A is required.

DESIGN PARAMETER	EXAMPLE VALUE
V _{S,nom}	5 V
V _{S,min}	4.9 V
I _{IN,FS}	±20 A

表 2. Example Application Design Requirements

10.2.2 Detailed Design Procedure

The primary design parameter for using theTMCS1101 is selecting the correct sensitivity variant, and because positive and negative current must be measured a bidirectional variant should be selected (A1B-A4B). Further consideration of noise and integration with an ADC can be explored, but is beyond the scope of this application design example. The TMCS1101AxB transfer function is effectively a transimpedance with a variable offset set by $V_{OUT.0A}$, which is internally set to half of the analog supply as defined by $\Delta \vec{x}$ 28.

 $V_{OUT} = I_{IN} \times S + V_{OUT.0A} = I_{IN} \times S + V_S \times .05$

(28)

Design of the sensing solution focuses on maximizing the sensitivity of the device while maintaining linear measurement over the expected current input range. The TMCS1101 has a slightly smaller linear output range to the supply than to ground; therefore, the measurable current range is always constrained by the positive swing to supply, Swing_{VS}. In order to account for the operating margin, consider the minimum possible supply voltage $V_{S,min}$. With the previous parameters, the maximum linear output voltage range is the range between $V_{OUT,max}$ and $V_{OUT,0A}$, as defined by $\Delta \vec{x}$ 29.

$$V_{OUT,max} - V_{OUT,0A} = V_{S,min} - Swing_{VS} - 0.5 \times V_{S,min}$$

(29)

Design parameters for this example application are shown in $\frac{1}{5}$ 3 along with the calculated output range.

	5
DESIGN PARAMETER	EXAMPLE VALUE
Swing _{VS}	0.2 V
V _{OUT,max}	4.7 V
V _{OUT,0A} at V _{S,min}	2.45 V
V _{OUT,max} – V _{OUT,0A}	2.25 V

表 3. Example Application Design Parameters

These design parameters result in a maximum positive linear output voltage swing of 2.25 V. To determine which sensitivity variant of the TMCS1101 most fully uses this linear range, calculate the maximum current range by Δ \vec{x} 30 for a bidirectional current (I_{B.MAX}).

IB,max = $(V_{OUT,max} - V_{OUT,0A}) / S_{A<x>}$

where

(30)

表 4 shows such calculation for each gain variant of the TMCS1101 with the appropriate sensitivities.

 $S_{A<x>}$ is the sensitivity of the relevant A1-A4 variant.

表 4. Maximum Full-Scale Current Ranges With 2.25-V Positive Output Swing

SENSITIVITY VARIANT	SENSITIVITY	I _{B,MAX}
TMCS1101A1B	50 mV/A	±45 A
TMCS1101A2B	100 mV/A	±22.5 A
TMCS1101A3B	200 mV/A	±11.25 A
TMCS1101A4B	400 mV/A	±5.6 A

In general, the highest sensitivity variant that provides for the desired full-scale current range is selected. For the design parameters in this example, the TMCS1101A2B with a sensitivity of 0.1 V/A is the proper selection because the maximum calculated ± 22.5 -A linear measurable range is sufficient for the desired ± 20 -A full-scale current.

The transfer function of the TMCS1101 linear sensing range for the nominal design parameters is shown in 14.



图 14. Application Example Design Transfer Curve

11 Power Supply Recommendations

The TMCS1101 only requires a power supply (V_S) on the low-voltage isolated side, which powers the analog circuitry independent of the isolated current input. V_S determines the full-scale output range of the analog output V_{OUT}, and can be supplied with any voltage between 3 V and 5.5 V. The TMCS1101 zero-current output voltage is derived from VS using a resistor divider; therefore, tale care to optimize the power supply path for both noise and stability across temperature to provide the highest precision measurement. To filter noise in the power-supply path, place a low-ESR decoupling capacitor of 0.1 uF between V_S and GND pins as close as possible to the supply and ground pins of the device. To compensate for noisy or high-impedance power supplies, add more decoupling capacitance.

12 Layout

12.1 Layout Guidelines

The TMCS1101 is specified for a continuous current handling capability of 20-A across the full ambient temperature range of -40°C to +125°C on the TMCS1100EVM, which uses 3-oz copper pour planes. This current capability is fundamentally limited by the maximum device junction temperature and the thermal environment, primarily the PCB layout and design. To maximize current-handling capability and thermal stability of the device, take care with PCB layout and construction to optimize the thermal capability. Efforts to improve the thermal performance beyond the design and construction of the TMCS1100EVM can result in increased continuous-current capability due to higher heat transfer to the ambient environment. Keys to improving thermal performance of the PCB include:

- Use large copper planes for both input current path and isolated power planes and signals.
- Use heavier copper PCB construction.
- Place thermal via *farms* around the isolated current input.
- Provide airflow across the surface of the PCB.

The TMCS1101 senses external magnetic fields, so make sure to minimize adjacent high-current traces in close proximity to the device. The input current trace can contribute additional magnetic field to the sensor if the input current traces are routed parallel to the vertical axis of the package. 15 illustrates the most optimal input current routing into the TMCS1101. As the angle that the current approaches the device deviates from 0° to the horizontal axis, the current trace contributes some additional magnetic field to the sensor, increasing the effective sensitivity of the device. If current must be routed parallel to the package vertical axis, move the routing away from the package to minimize the impact to the sensitivity of the device. Terminate the input current path directly underneath the package lead footprint, and use a merged copper input trace for both the IN+ and IN– inputs.



图 15. Magnetic Field Generated by Input Current Trace



Layout Guidelines (接下页)

In addition to thermal and magnetic optimization, make sure to consider the PCB design required creepage and clearance for system-level isolation requirements. Maintain required creepage between solder stencils, as shown in 🛽 16, if possible. If not possible to maintain required PCB creepage between the two isolated sides at board level, add additional slots or grooves to the board. If more creepage and clearance is required for system isolation levels than is provided by the package, the entire device and solder mask can be encapsulated with an overmold compound to meet system-level requirements.



图 16. Layout for System Creepage Requirements

12.2 Layout Example

An example layout, shown in 🛿 17, is from the TMCS1101EVM. Device performance is targeted for thermal and magnetic characteristics of this layout, subject to change.



图 17. Recommended Board Top (Left) and Bottom (Right) Plane Layout

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13 器件和文档支持

- 13.1 器件支持
- 13.1.1 开发支持
 - 要获得开发工具支持,请参阅以下文档:
 - TMCS1101EVM
 - TMCS1101 TI-TINA 模型
 - TMCS1101 TINA-TI 参考设计

13.2 文档支持

13.2.1 相关文档

请参阅如下相关文档:

- 德州仪器 (TI), 《TMCS1101EVM 用户指南》
- 德州仪器 (TI), 《使用非比例式磁性电流传感器进行精密电流感应设计》
- 德州仪器 (TI), 《低漂移、高精度、直插式隔离式磁性电机电流测量》
- 德州仪器 (TI), 《隔离相关术语》

13.3 接收文档更新通知

要接收文档更新通知,请导航至 ti.com. 上的器件产品文件夹。单击右上角的通知我进行注册,即可每周接收产品 信息更改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

13.4 支持资源

TI E2E[™] support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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13.5 商标

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13.6 静电放电警告



ESD 可能会损坏该集成电路。德州仪器 (TI) 建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序,可能会损坏集成电路。

ESD 的损坏小至导致微小的性能降级,大至整个器件故障。精密的集成电路可能更容易受到损坏,这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

13.7 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

14 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。数据如有变更,恕不另行通知,且 不会对此文档进行修订。如需获取此数据表的浏览器版本,请查阅左侧的导航栏。

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10-Dec-2020

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TMCS1101A1BQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	(6) SN	Level-2-260C-1 YEAR	-40 to 125	M01A1B	Samples
TMCS1101A1BQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A1B	Samples
TMCS1101A1UQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A1U	Samples
TMCS1101A1UQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A1U	Samples
TMCS1101A2BQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A2B	Samples
TMCS1101A2BQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A2B	Samples
TMCS1101A2UQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A2U	Samples
TMCS1101A2UQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A2U	Samples
TMCS1101A3BQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A3B	Samples
TMCS1101A3BQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A3B	Samples
TMCS1101A3UQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A3U	Samples
TMCS1101A3UQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A3U	Samples
TMCS1101A4BQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A4B	Samples
TMCS1101A4BQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A4B	Samples
TMCS1101A4UQDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A4U	Samples
TMCS1101A4UQDT	ACTIVE	SOIC	D	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	M01A4U	Samples

⁽¹⁾ The marketing status values are defined as follows: **ACTIVE:** Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.



10-Dec-2020

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

⁽³⁾ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

⁽⁴⁾ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

⁽⁵⁾ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION





QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal												
Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TMCS1101A1BQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A1BQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A1UQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A1UQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A2BQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A2BQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A2UQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A2UQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A3BQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A3BQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A3UQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A3UQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A4BQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A4BQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A4UQDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TMCS1101A4UQDT	SOIC	D	8	250	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

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PACKAGE MATERIALS INFORMATION

20-Jun-2020



*All dimensions are nominal	1				1		1
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TMCS1101A1BQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A1BQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A1UQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A1UQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A2BQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A2BQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A2UQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A2UQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A3BQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A3BQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A3UQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A3UQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A4BQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A4BQDT	SOIC	D	8	250	350.0	350.0	43.0
TMCS1101A4UQDR	SOIC	D	8	2500	350.0	350.0	43.0
TMCS1101A4UQDT	SOIC	D	8	250	350.0	350.0	43.0

D0008A



PACKAGE OUTLINE

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



D0008A

EXAMPLE BOARD LAYOUT

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



D0008A

EXAMPLE STENCIL DESIGN

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.



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